

Supplementary material
for
**Microstructure modulation of α -MnO₂ via mild urea-induced phase transition
for enhanced catalytic ozonation of emerging contaminants**

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Contents

Text S1. Removal calculation method

Text S2. Preparation detail of simulated wastewater for water matrices assessment

Text S3. Semi-quantitative analysis of mass ratio of α -MnO₂ and Mn₃O₄

Fig. S1. Laboratory setup of catalytic ozonation system.

Fig. S2. TG-MS curves of urea pyrolysis process.

Fig. S3. XRD patterns of Mn300-0.125U.

Fig. S4. (a–c) TEM and HRTEM images of Mn400-0U (α -MnO₂); (d–f) TEM and HRTEM images of Mn400-0.25U (Mn₃O₄).

Fig. S5. (a) Removal of SMZ and (b) pseudo first-order kinetics fitting for SMZ removal in O₃/Mn200-0.125U, O₃/Mn300-0.125U and O₃/Mn400-0.125U systems.

Fig. S6. Comparison of different commercial catalysts with Mn400-0.125U in the catalytic ozonation system: (a) removal of SMZ and (b) pseudo first-order kinetics fitting for SMZ removal.

Fig. S7. XRD patterns of Mn400-0.125U before and after reaction.

Fig. S8. TEM images of Mn400-0.125U (α -MnO₂/Mn₃O₄) after cycled reaction.

Fig. S9. XPS spectra of Mn 2p (a) and O 1s (b) Mn400-0.125U before and after reaction.

Table S1. BET surface area of different catalysts.

Text S1. Removal rate calculation method

The formula for calculating the sulfamethoxazole (SMZ) removal is defined as follows:

$$\text{Removal (\%)} = (C_0 - C_t) / C_0 \times 100\%$$

Where C_0 is the initial concentration of SMZ, and C_t is the concentration of SMZ at a specific reaction time t . All measurements were repeated in triplicate and reported as the average values.

Text S2. Preparation detail of simulated wastewater for water matrices assessment

To assess the effect of diverse anions (e.g., Cl^- , NO_3^- , SO_4^{2-} , HCO_3^{2-} and $\text{H}_2\text{PO}_4^{2-}$) and humic acid (HA) on SMZ removal, catalytic ozonation experiments were conducted with simulated wastewater. The simulated wastewater was prepared by adding specific salts to deionized water to achieve the desired background anion concentration. The concentration of each anion and HA was set as: Cl^- (100 mM), NO_3^- (100 mM), SO_4^{2-} (100 mM), HCO_3^{2-} (10 mM), $\text{H}_2\text{PO}_4^{2-}$ (10 mM) and HA (10 mg/L), respectively. A specific amount of sulfamethoxazole was then added to complete the preparation of each simulated wastewater.

Text S3. Semi-quantitative analysis of mass ratio of α -MnO₂ and Mn₃O₄

The reference intensity ratio (RIR) value of α -MnO₂ was first determined to be 0.527 using the internal standard method, where the samples were blended with a 1:1 mass ratio of corundum (α -Al₂O₃, JCPDS 46-1212) [1]. The RIR of Mn₃O₄ was 1.50 adopted directly from JCPDS 24-0734. The mass fractions of α -MnO₂ (W_A) and Mn₃O₄ (W_B) were then calculated using the equation:

$$W_A / W_B = (I_A / I_B) \times (K_B / K_A)$$

where I_A and I_B are the strongest peak intensity of α -MnO₂ and Mn₃O₄, respectively, which can be calculated based on the XRD patterns using Jade software. And K_A and K_B are their RIR values.

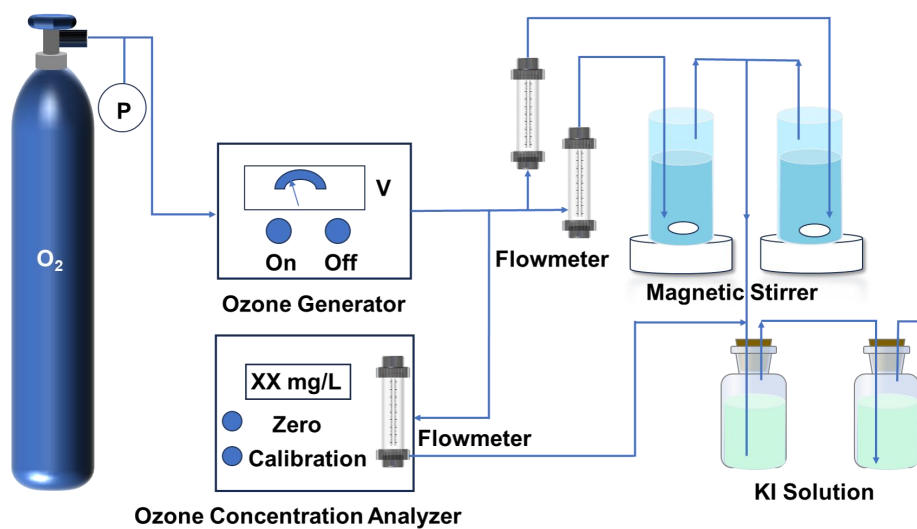


Fig. S1. Laboratory setup of catalytic ozonation system.

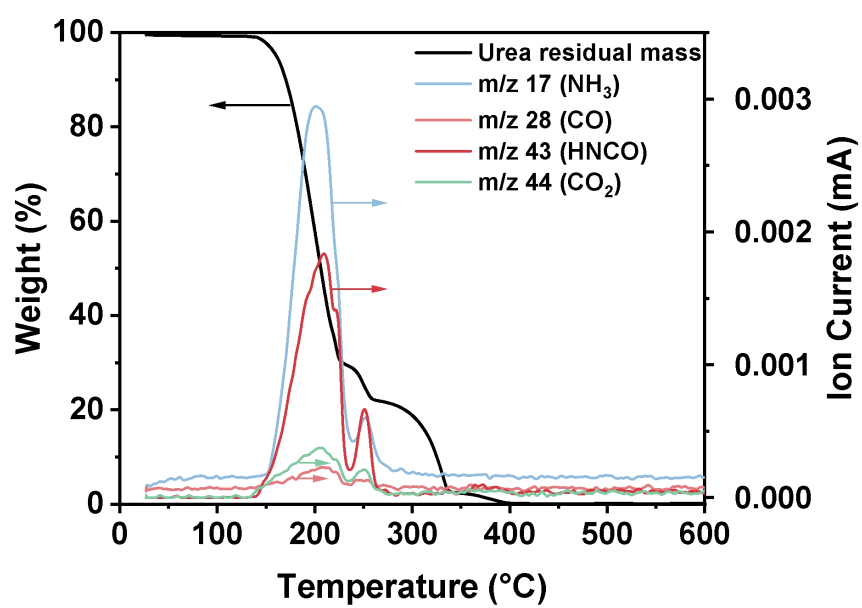


Fig. S2. TG-MS curves of urea pyrolysis process.

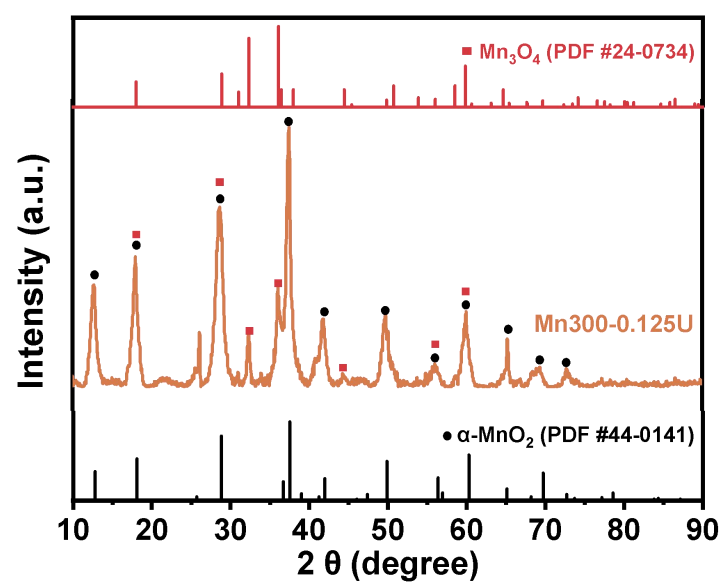


Fig. S3. XRD patterns of Mn300-0.125U.

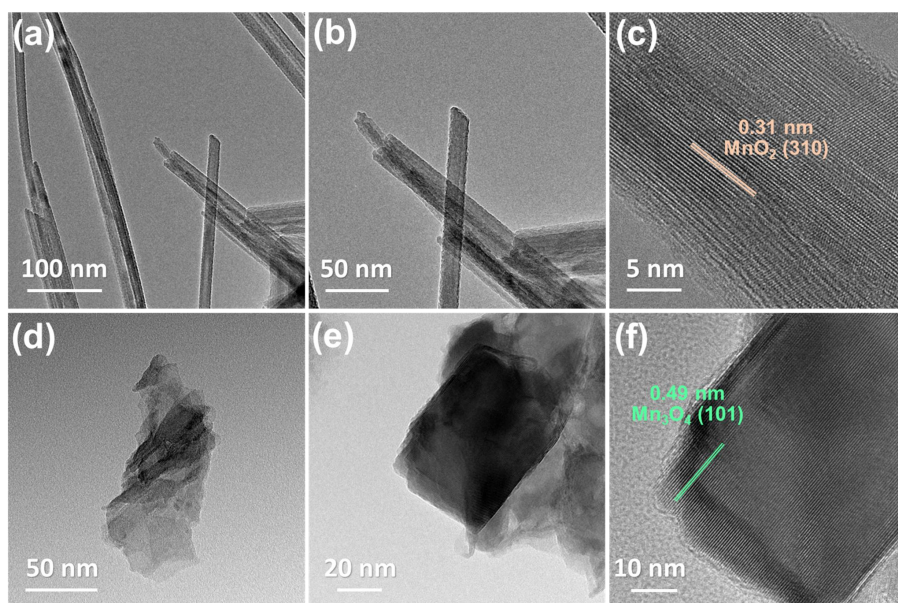


Fig. S4. (a–c) TEM and HRTEM images of Mn400-0U (α -MnO₂); (d–f) TEM and HRTEM images of Mn400-0.25U (Mn₃O₄).

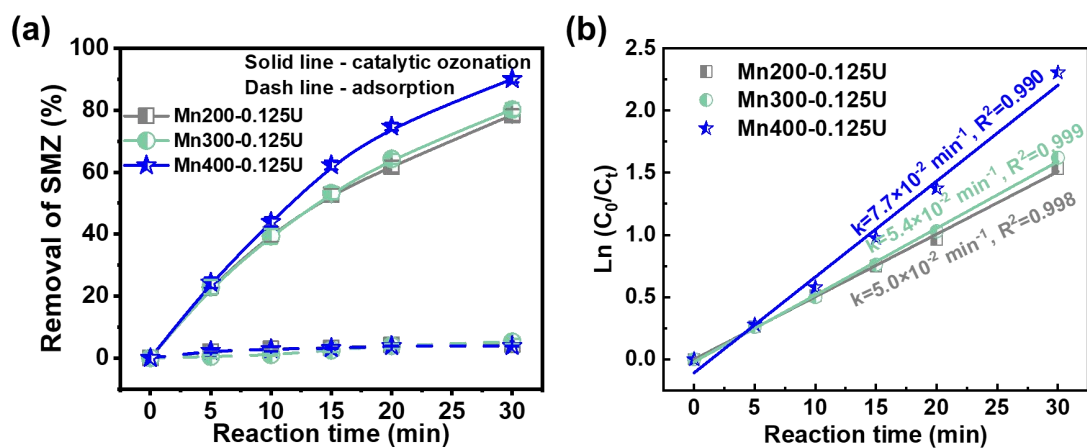


Fig. S5. (a) Removal of SMZ and (b) pseudo first-order kinetics fitting for SMZ removal in $\text{O}_3/\text{Mn200-0.125U}$, $\text{O}_3/\text{Mn300-0.125U}$ and $\text{O}_3/\text{Mn400-0.125U}$ systems.

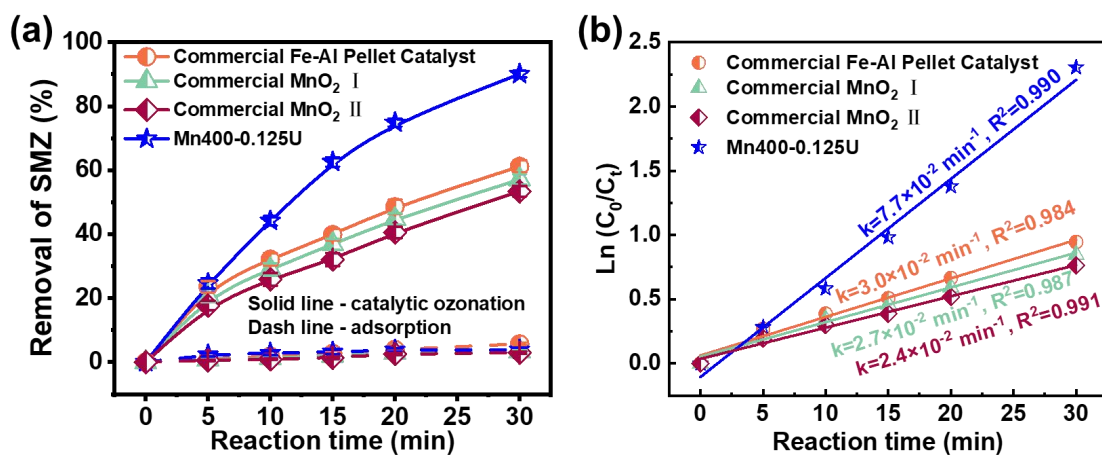


Fig. S6. Comparison of different commercial catalysts with Mn400-0.125U in the catalytic ozonation system: (a) removal of SMZ and (b) pseudo first-order kinetics fitting for SMZ removal. Commercial MnO₂ I was purchased from Tianjin Fuchen Chemical Reagent Factory, commercial MnO₂ II was purchased from Tianjin Damao Chemical Reagent Factory, and commercial Fe-Al pellet catalyst was purchased from Pingxiang Rongjian Environmental Protection Chemical Packing Co., Ltd.

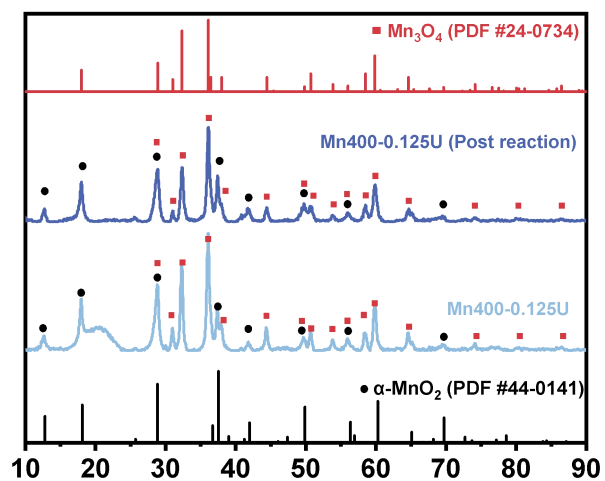


Fig. S7. XRD patterns of Mn400-0.125U before and after reaction.

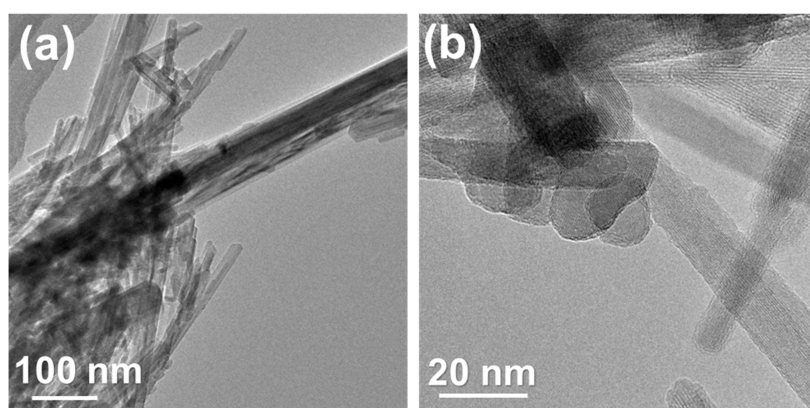


Fig. S8. TEM images of Mn400-0.125U (α -MnO₂/Mn₃O₄) after cycled reaction.

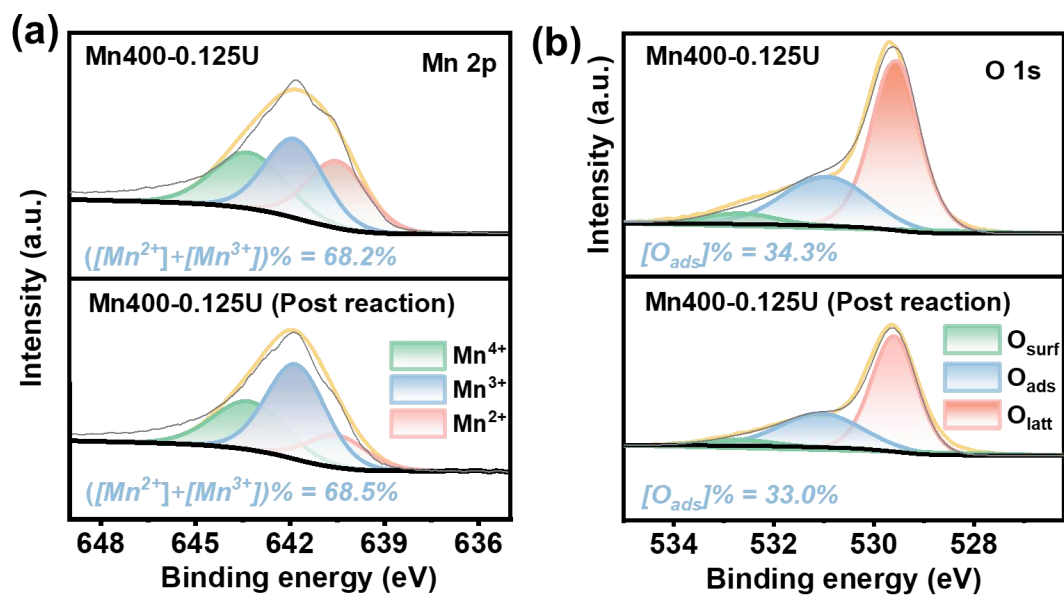


Fig. S9. XPS spectra of Mn 2p (a) and O 1s (b) Mn400-0.125U before and after reaction.

Table S1. BET surface area of different catalysts.

Samples	BET surface area (m ² /g)
α -MnO ₂	91.13
Mn400-0U	70.90
Mn400-0.125U	44.06
Mn400-0.250U	47.19

Reference

- [1] W.Q. Li, Z.H. Wen, S.H. Tian, L.J. Shan, Y. Xiong, *Catal. Sci. Technol.*, **2018**, 8, 1051-1061.